

THE PROBLEM OF EXISTENCE THE NEUTRAL SURFACE FOR THE ELASTIC  
SHELL \*

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**Abstract.** I. Vekua obtained the conditions for the existence of the neutral surface of a shell, when the neutral surface is the middle surface. In this paper the neutral surface is considered as any equidistant surfaces of the shell.

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The stress-strain relations are given in the form [1, 2]

$$\sigma_j^i = \lambda\theta g_j^i + 2\mu e_j^i, \quad (i, j = 1, 2, 3), \quad (1)$$

where  $\sigma_j^i$  and  $e_j^i$  are the mixed components, respectively of stress and strain tensors,  $\theta$  is the cubical dilatation which will be written as

$$\theta = \theta' + e_3^3, \quad \theta' = e_\alpha^\alpha, \quad (\alpha = 1, 2). \quad (2)$$

when  $j = 3$  from (1) we have

$$\sigma_3^\alpha = 2\mu e_3^\alpha, \quad \sigma_3^3 = \lambda\theta + 2\mu e_3^3 = \lambda\theta' + (\lambda + 2\mu)e_3^3. \quad (3)$$

From (3)

$$e_3^\alpha = \frac{1}{2\mu}\sigma_3^\alpha, \quad e_3^3 = -\frac{\lambda}{\lambda + 2\mu}\theta' + \frac{1}{\lambda + 2\mu}\sigma_3^3. \quad (4)$$

By inserting (4) into (2) we obtain

$$\theta = \frac{\lambda'}{\lambda}\theta' + \frac{1}{\lambda + 2\mu}\sigma_3^3, \quad \lambda' = \frac{2\lambda\mu}{\lambda + 2\mu}. \quad (5)$$

Substituting expression (5) into (1) we get

$$\sigma_j^i = T_j^i + Q_j^i = \left( \lambda'\theta' + \frac{\lambda}{\lambda + 2\mu}\sigma_3^3 \right) g_j^i + 2\mu e_j^i,$$

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where

$$T_\beta^\alpha = \lambda' \theta g_\beta^\alpha + 2\mu e_\beta^\alpha, \quad Q_\beta^\alpha = \sigma' \sigma_3^3 g_\beta^\alpha, \quad T_3^i = 0, \quad Q_3^i = \sigma_3^i, \quad \left( \sigma' = \frac{\lambda}{\lambda + 2\mu} \right). \quad (6)$$

The vector  $\mathbf{T}^\alpha$  satisfies the condition  $\mathbf{nT}^\alpha = 0$  and is therefore called the tangential stress field and the vector  $\mathbf{Q}^i$  will be called the transverse field.

The vectorial equation of equilibrium

$$\frac{1}{\sqrt{g}} \partial_i (\sqrt{g} \sigma^i) + \Phi = 0, \quad (\sqrt{g} = \sqrt{a} \vartheta, \quad \vartheta = 1 - 2Hx_3 + Kx_3^2) \quad (7)$$

may be written as

$$\frac{1}{\sqrt{g}} [\partial_\alpha (\sqrt{g} \mathbf{T}^\alpha) + \partial_i (\sqrt{g} \mathbf{Q}^i)] + \Phi = 0. \quad (8)$$

Let the surface  $\hat{S} : x^3 = \text{const}$  be the neutral surface of a non-shallow shell. Then  $\mathbf{T}^\alpha = 0$ , i.e.  $T^{\alpha\beta} = 0$  (on  $\hat{S}$ ), and equation (8)

$$\frac{1}{\sqrt{a}} \partial_\alpha (\sqrt{a} \vartheta \mathbf{Q}^\alpha) + \partial_3 (\vartheta \sigma^3) + \vartheta \Phi = 0,$$

or

$$[\nabla_\alpha (\vartheta \mathbf{Q}^\alpha) + \partial_3 (\vartheta \sigma^3) + \vartheta \Phi]_{x^3=\text{const}} = 0, \quad (-h \leq x^3 = x_3 \leq h) \quad (9)$$

where  $2h$  is the thickness of the shell and

$$\mathbf{Q}^\alpha = \sigma' \sigma_3^3 \mathbf{R}^\alpha + \sigma_3^\alpha \mathbf{n}, \quad \nabla_\alpha (\cdot) = \frac{1}{\sqrt{a}} \partial_\alpha (\sqrt{a} \cdot). \quad (10)$$

Denote the stress forces acting on the face surfaces  $S^+$  and  $S^-$  by  $\mathbf{P}^{(+)}$  and  $\mathbf{P}^{(-)}$ . We have

$$\mathbf{P}^{(+)} = -(\sigma^3)_{x^3=h}, \quad \mathbf{P}^{(-)} = (\sigma^3)_{x^3=-h}. \quad (11)$$

If we approximately represent  $\sigma^3$  by the formula

$$\sigma^3(x^1, x^2, x^3) \cong \sigma^0(x^1, x^2) + x^3 \sigma^1(x^1, x^2). \quad (12)$$

from (11) we get

$$\begin{aligned} \sigma^3(x^1, x^2, x^3) &\cong -\frac{1}{2} \left[ \mathbf{P}^{(+)} - \mathbf{P}^{(-)} + \frac{x^3}{h} \left( \mathbf{P}^{(+)} + \mathbf{P}^{(-)} \right) \right] \\ &= -\frac{1}{2} \left[ \frac{h+x_3}{h} \left( \mathbf{P}^{(+)} - \mathbf{P}^{(-)} \right) + \frac{2x^3}{h} \mathbf{P}^{(-)} \right], \end{aligned} \quad (13)$$

or

$$\sigma^3(x^1, x^2, x^3) = -\frac{1}{2} \left[ \frac{h+x_3}{h} \left( P^\alpha \mathbf{r}_\alpha + P^3 \mathbf{n} \right) + \frac{2x^3}{h} \mathbf{P}^{(-)} \right], \quad (14)$$

$$P^\alpha = \overset{(+)}{P}^\alpha - \overset{(-)}{P}^\alpha, \quad P = \overset{(+)}{P}^3 - \overset{(-)}{P}^3.$$

Then to define the vector field  $\overset{(+)}{\mathbf{P}}$  we have the equation

$$\left\{ \nabla_\alpha (\sigma' A_\beta^\alpha P \mathbf{r}^\beta + A P^\alpha \mathbf{n}) + B(P \mathbf{n} + P^\alpha \mathbf{r}_\alpha) + \tilde{\Phi} \right\}_{x^3=c} = 0 \quad (15)$$

where

$$\begin{aligned} A_\beta^\alpha &= \frac{h+c}{h} [a_\beta^\alpha + c(b_\beta^\alpha - 2H a_\beta^\alpha)], \quad A = \frac{h+c}{h} \vartheta(c), \\ B &= \frac{1}{h} [1 - 2Hh + 2(Kh - 2H)c + 3Kc^2], \\ \tilde{\Phi} &= -2\vartheta(c)\Phi(c) + \nabla_\alpha \left\{ \sigma' \frac{2c}{h} [a_\beta^\alpha + c(b_\beta^\alpha - 2H a_\beta^\alpha)] \overset{(-)}{P}^\beta \mathbf{r}^\beta + \frac{2c}{h} \vartheta(c) \overset{(-)}{P}^\alpha \mathbf{n} \right\} \\ &+ \frac{2}{h} [\vartheta(c) + 2(Kc - H)] \overset{(-)}{\mathbf{P}}. \end{aligned} \quad (16)$$

Since

$$\nabla_\alpha \mathbf{r}^\beta = b_\alpha^\beta \mathbf{n}, \quad \text{and} \quad \nabla_\alpha \mathbf{n} = -b_{\alpha\beta} \mathbf{r}^\beta$$

from (15) we have

$$\sigma' \nabla_\alpha (A_\beta^\alpha P) + (B a_{\alpha\beta} - A b_{\alpha\beta}) P^\alpha + \tilde{\Phi}_\beta = 0, \quad (\tilde{\Phi}_\beta = \tilde{\Phi} \mathbf{r}_\beta), \quad (17)$$

$$\nabla_\alpha (A P^\alpha) + (\sigma' A_\beta^\alpha b_\alpha^\beta + B) P + \tilde{\Phi}_3 = 0, \quad (\tilde{\Phi}_3 = \tilde{\Phi} \mathbf{n}). \quad (18)$$

From the system of equations (17) we have

$$P^\alpha = \overset{(+)}{P}^\alpha - \overset{(-)}{P}^\alpha = -\hat{d}^{\alpha\beta} \left[ \nabla_\alpha (A_\beta^\alpha P) + \tilde{\Phi}_\beta \right], \quad (19)$$

where

$$\begin{aligned} \hat{d}^{\alpha\beta} &= \frac{1}{\Delta} [(B - 2AH) a^{\alpha\beta} + A b^{\alpha\beta}], \quad \hat{F}_\beta = - \left[ \tilde{\Phi}_\beta + \nabla_\alpha (A_\beta^\alpha P) \right], \\ \Delta &= B^2 - 2ABH + A^2K. \end{aligned} \quad (20)$$

Inserting expressions (19) into (18) we obtain the equation

$$\sigma' \nabla_\alpha \left[ A \hat{d}^{\alpha\beta} \nabla_\gamma (A_\beta^\alpha P) \right] - (B + \sigma' A_\beta^\alpha b_\alpha^\beta) P + \Phi = 0. \quad (21)$$

It is easily seen that equation (21) is of the elliptic type.

Thus, if the surface  $x^3 = c$  is neutral, the stress  $\overset{(+)}{\mathbf{P}}$  and  $\overset{(-)}{\mathbf{P}}$ , applied to the face surfaces, must satisfy the vector equation (17) and (18). This means that the stresses  $\overset{(+)}{\mathbf{P}}$  and  $\overset{(-)}{\mathbf{P}}$  cannot be prescribed arbitrarily both at the same time. However there are problems when this does not occur. For example, in aircraft or submarine apparatus the force  $\overset{(-)}{\mathbf{P}}$

acting on the inner surface  $S^-$  may be assumed to be prescribed, but the  $\mathbf{P}^{(+)}$  acting on the external face surface  $S^+$  is not, in general, assigned beforehand. The same situation occurs on dams. One face surface of the dam is free from stresses and the other is under the hydrodynamic load, a variable which is generally difficult to define exactly at any moment in time.

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